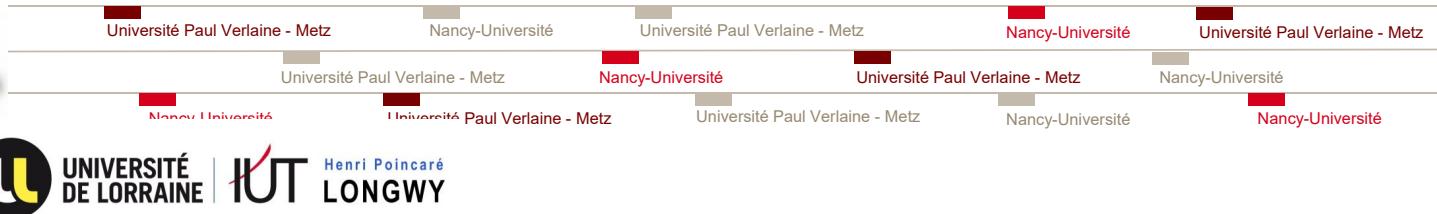
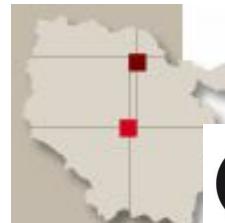


Africa-Europe BioClimatic buildings for XXI century

The International Conference on Bioclimatic Materials and Buildings:
Energy efficiency and global industry value chain, ICBMB

Université de Lorraine



Professor M. El Ganaoui, University of Lorraine, France

Recherche en énergétique @ Longwy



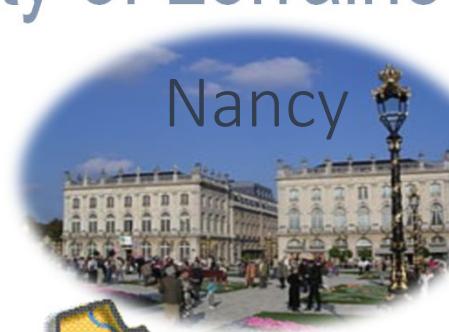
Mohammed.el-ganaoui@univ-lorraine.fr



University of Lorraine



Nancy



Metz



Longwy



Nancy



Epinal

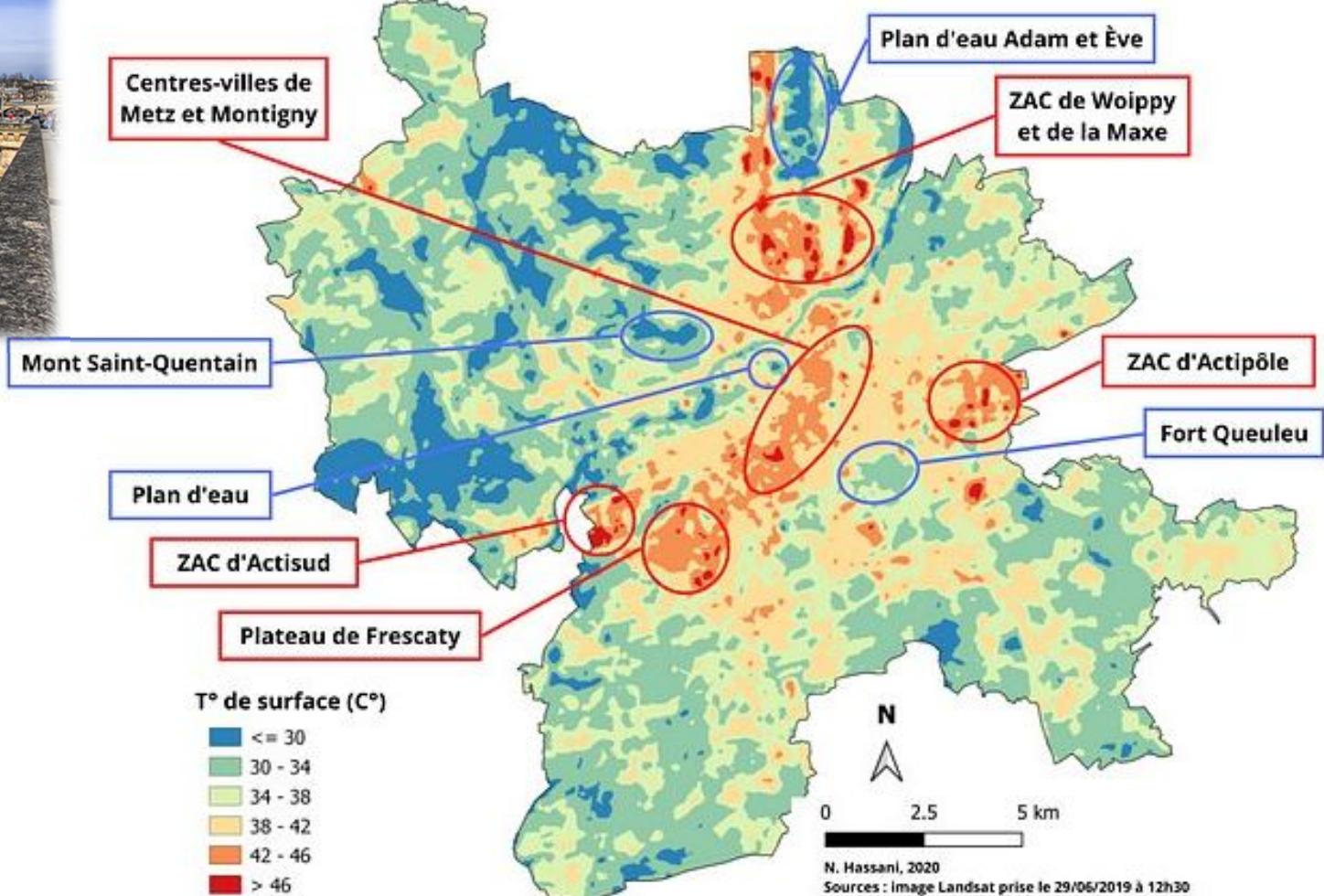




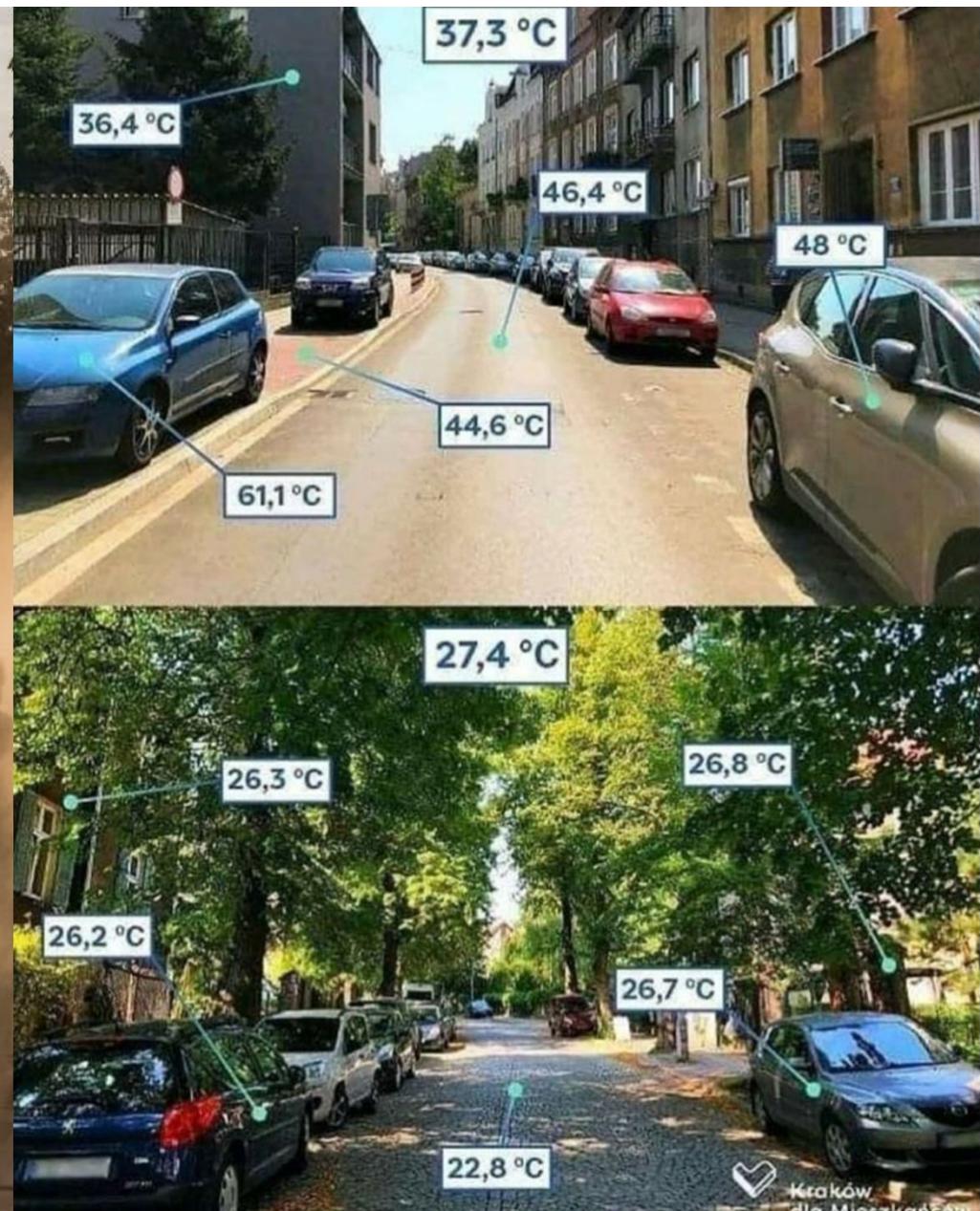
Last summer
 > 3 ° Centre to Green peripherie



Exchange with Phd student Nassima Hassani







The Rodney & Otamatea Times

WAITEMATA & KAIPARA GAZETTE.

PRICE—10s per annum in advance

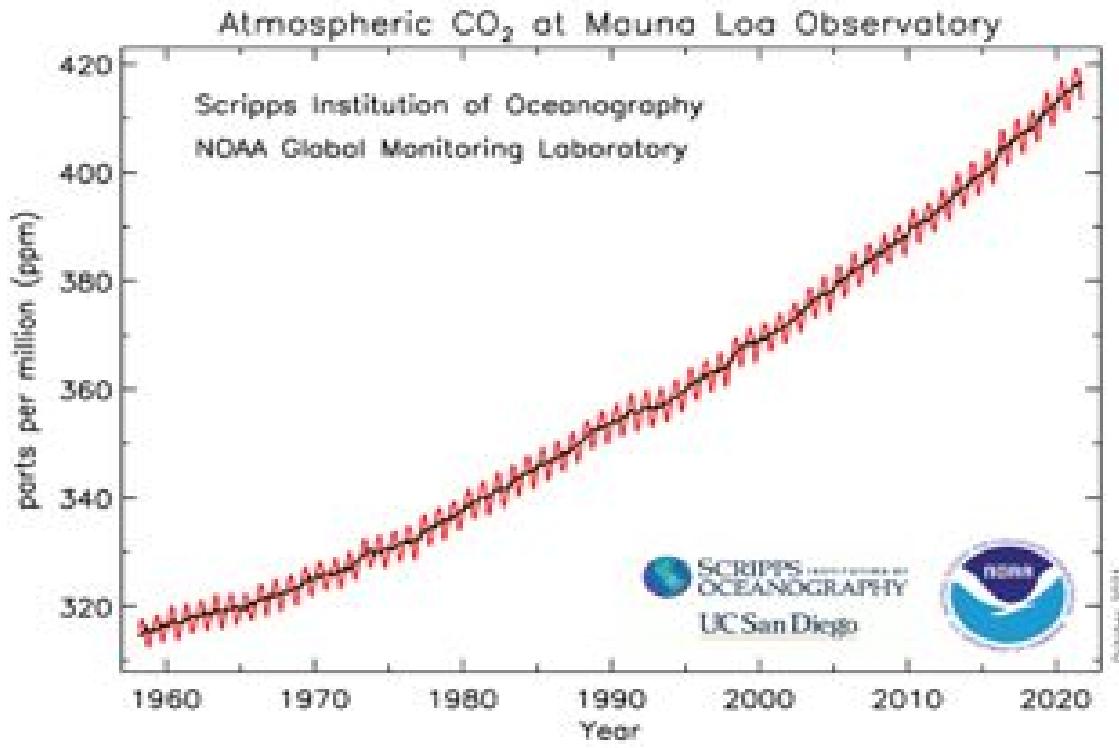
WARKWORTH, WEDNESDAY, AUGUST 14, 1912.

3d. per Copy.

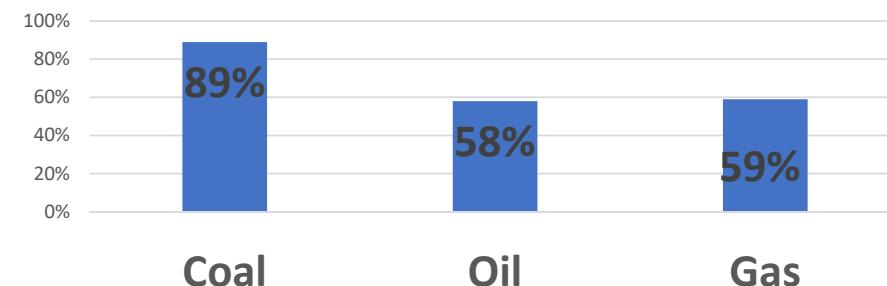
Science Notes and News.

COAL CONSUMPTION AFFECTING CLIMATE.

The furnaces of the world are now burning about 2,000,000,000 tons of coal a year. When this is burned, uniting with oxygen, it adds about 7,000,000,000 tons of carbon dioxide to the atmosphere yearly. This tends to make the air a more effective blanket for the earth and to raise its temperature. The effect may be considerable in a few centuries.



Fossil fuel to be left in the ground to keep to 1.5C limit



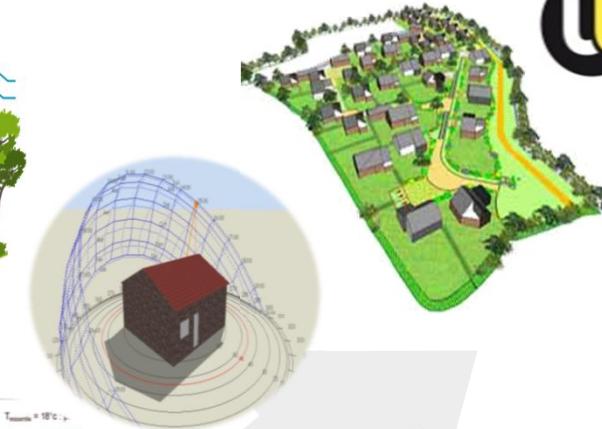
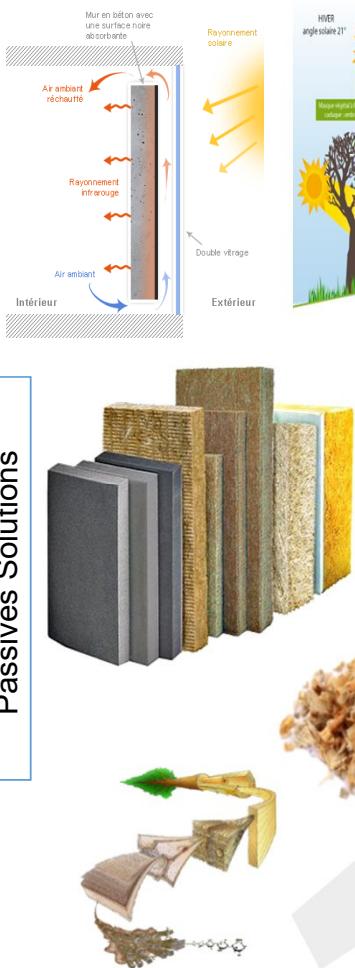
The challenge of staying below the 1.5°C is unlikely to be met

Morocco is now in 7th position in the Climate Change Performance Index indicating its potential and development.

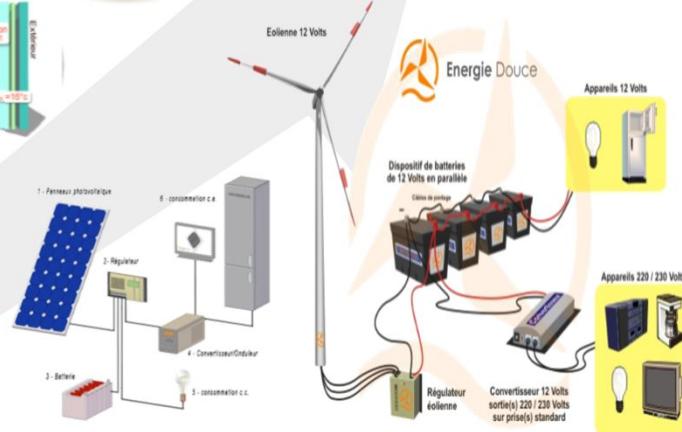
Geoffry Levermore at the Academy Talk November 2022.
Climate change and the net zero challenge



Passives Solutions

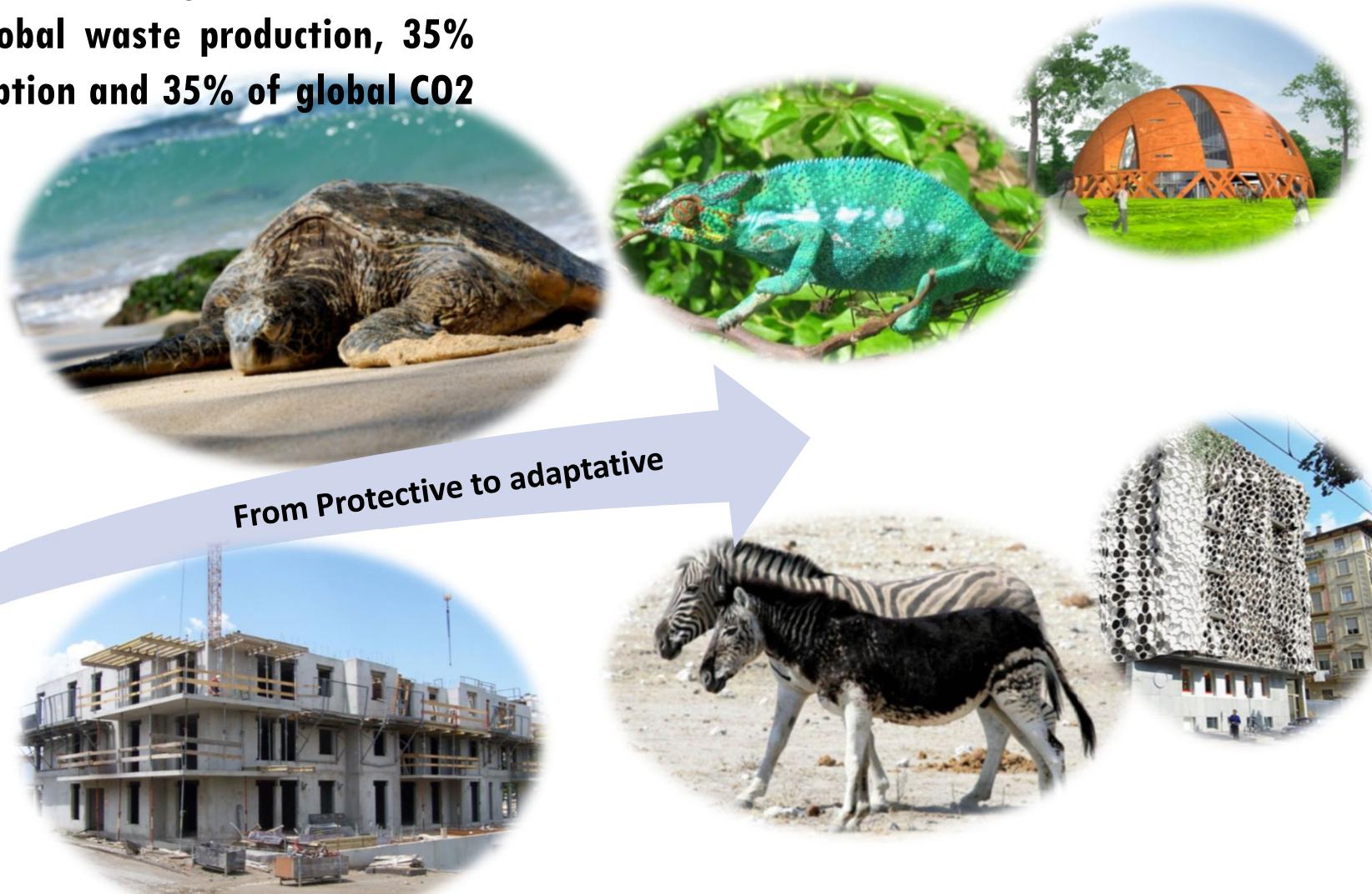


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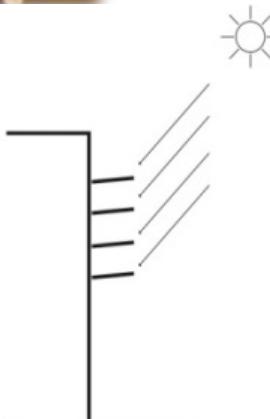
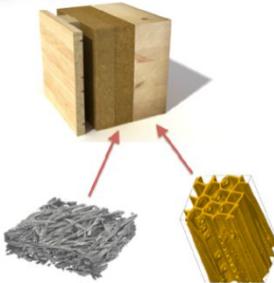
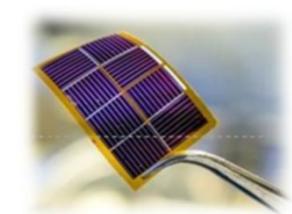
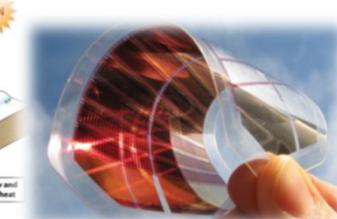
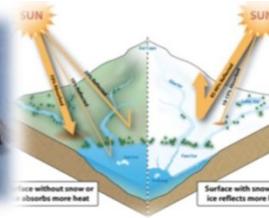


Active Solutions

Building/environment: 60% of global resources consumption, 50% of global waste production, 35% of global energy consumption and 35% of global CO₂ emissions.



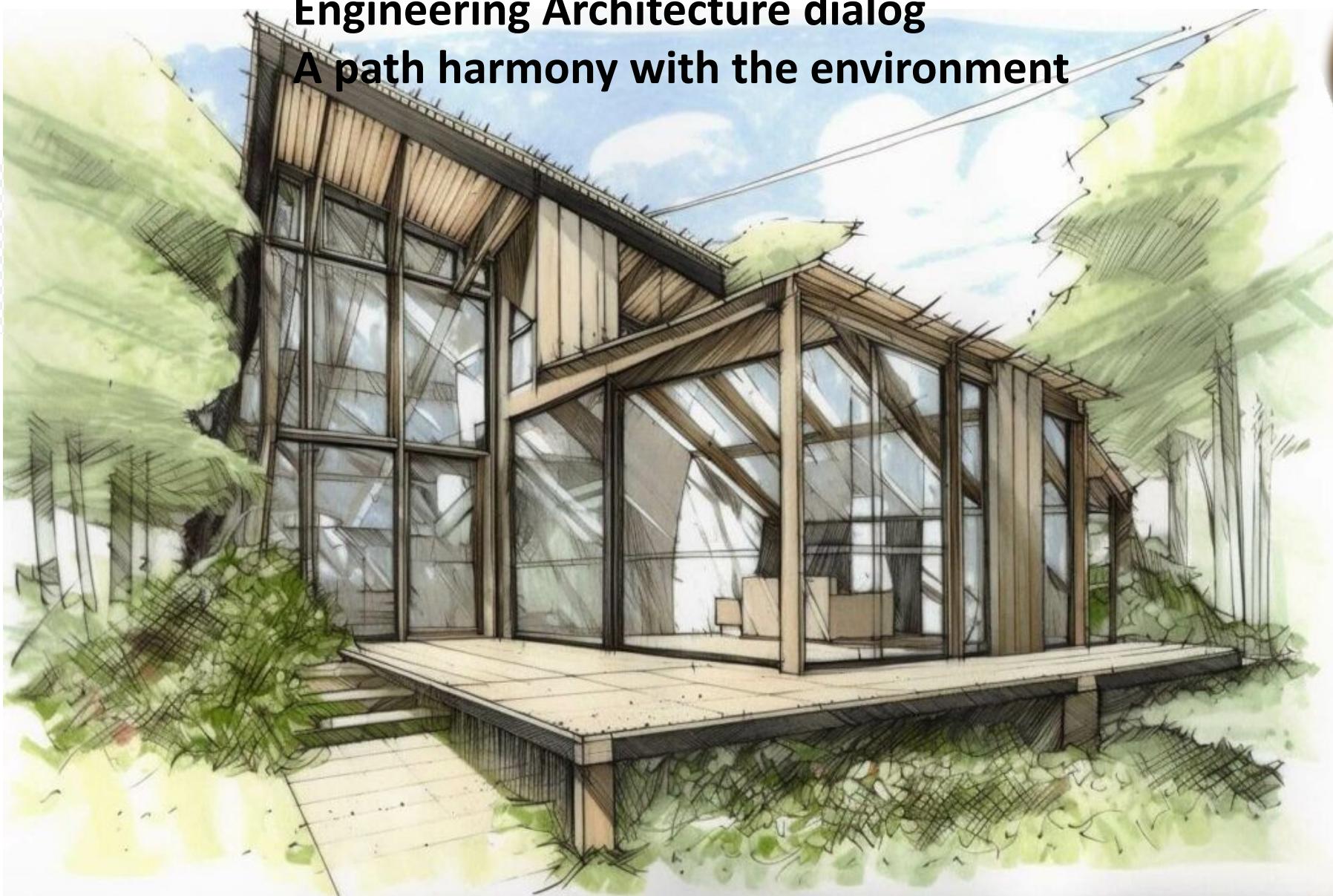
Nature exhibits many possibilities of adaptation that architects and specialists on buildings are considering



Récupération des eaux de pluies

Engineering Architecture dialog

A path harmony with the environment

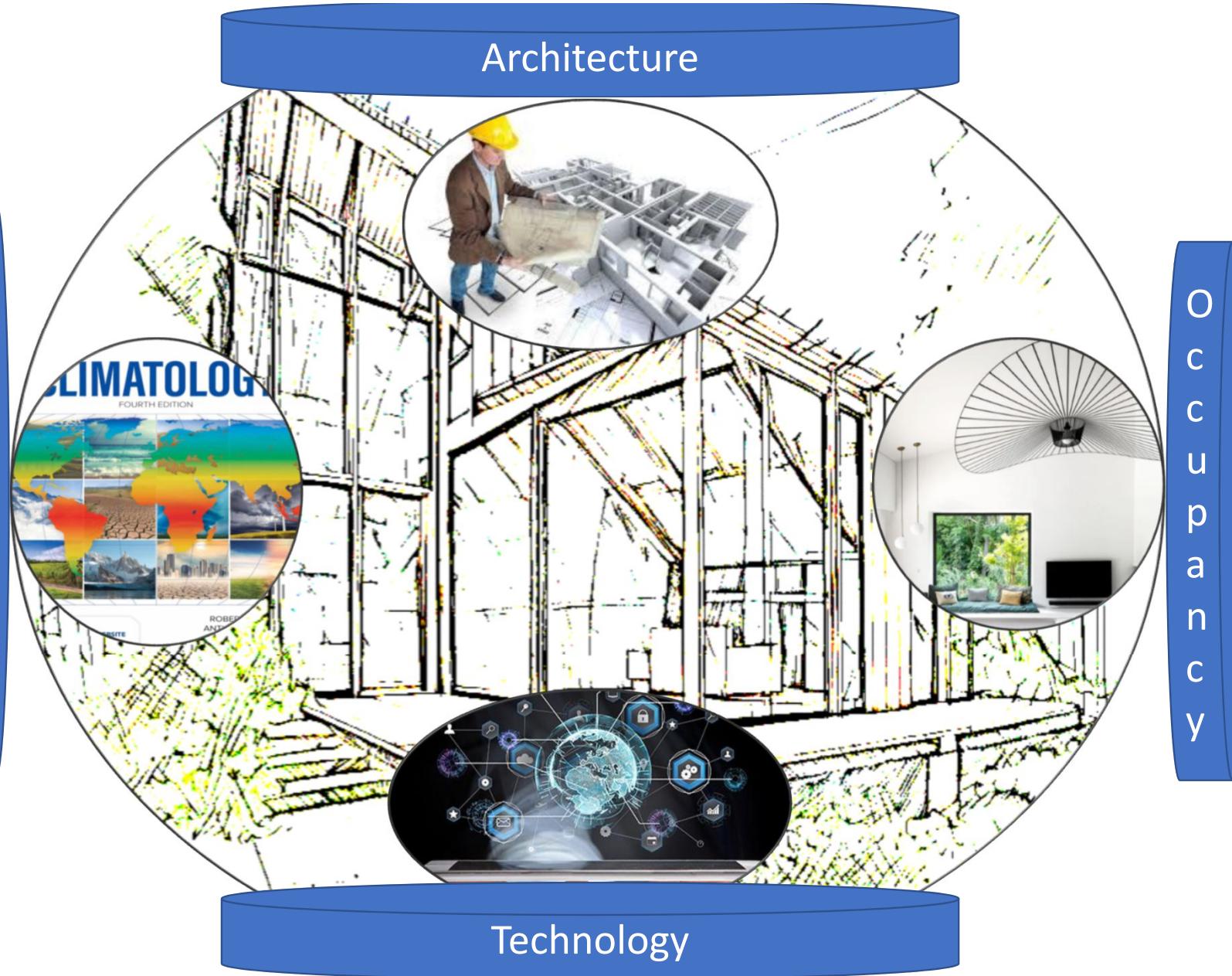


Climatology

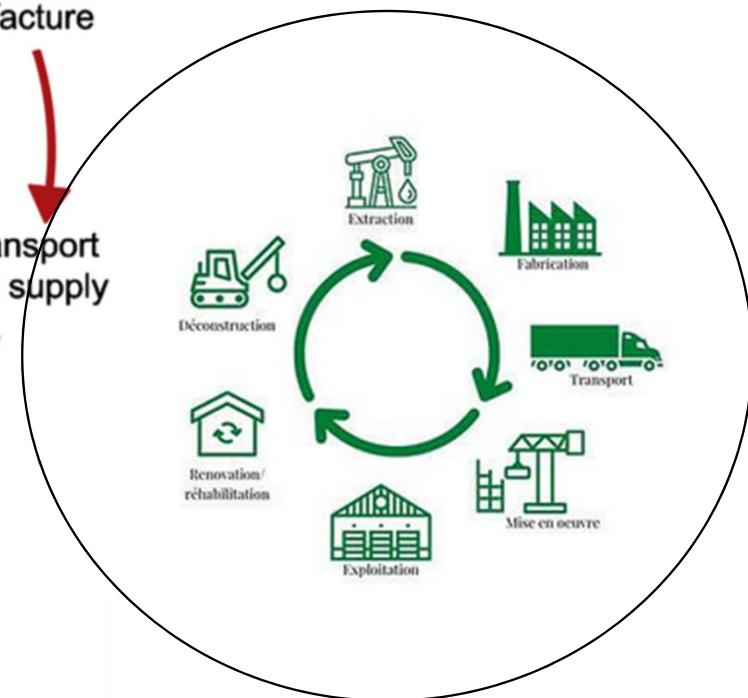
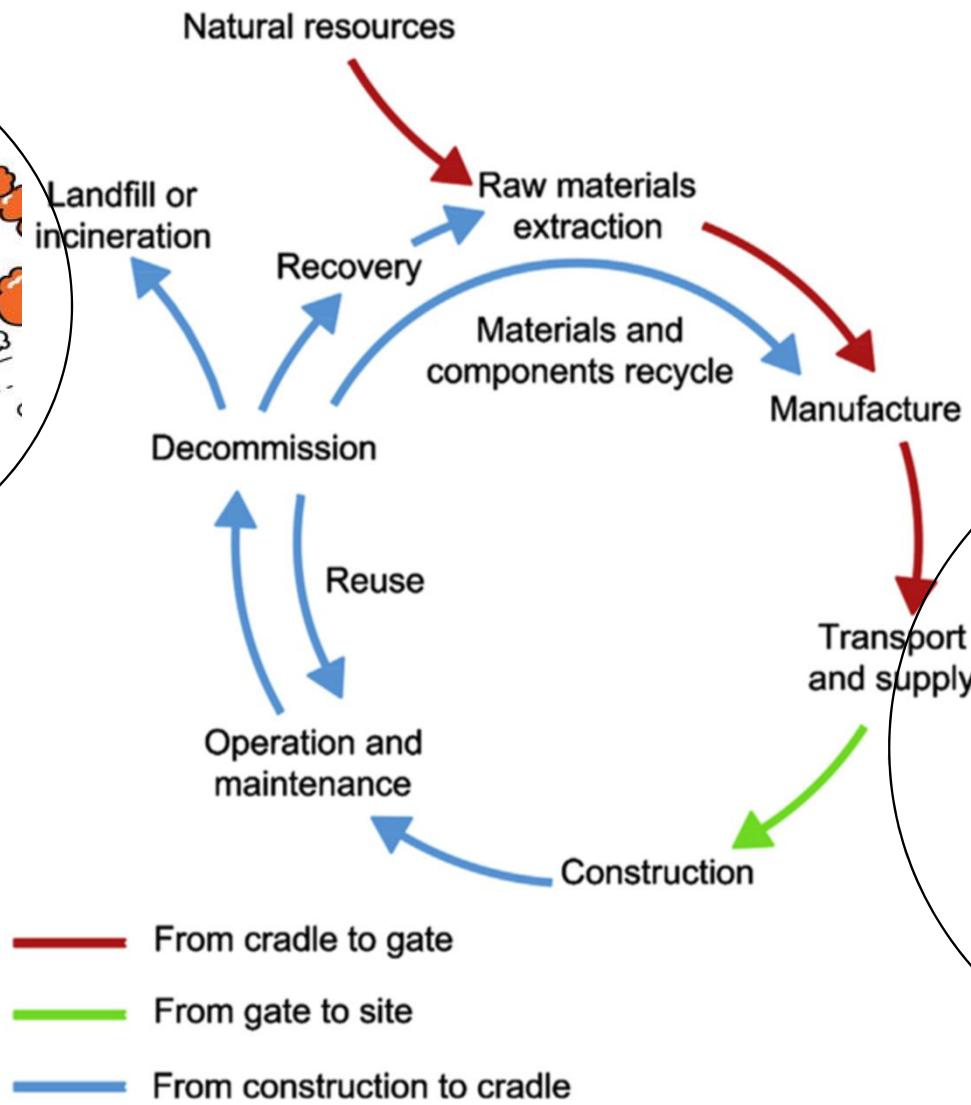
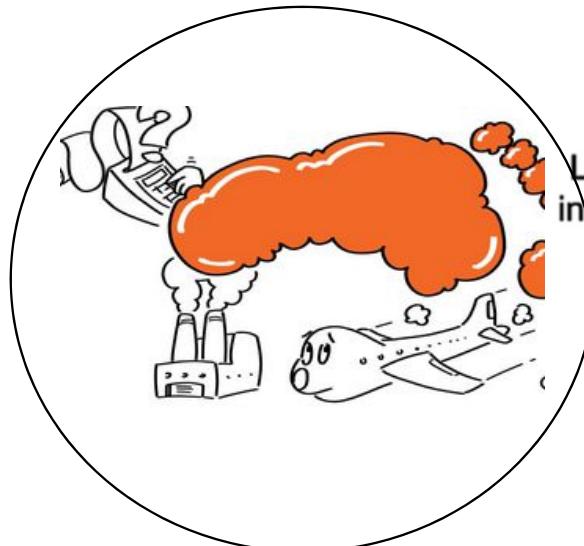
Architecture

Occupancy

Technology



Life cycle of building Materials and Products



Wood A promising material



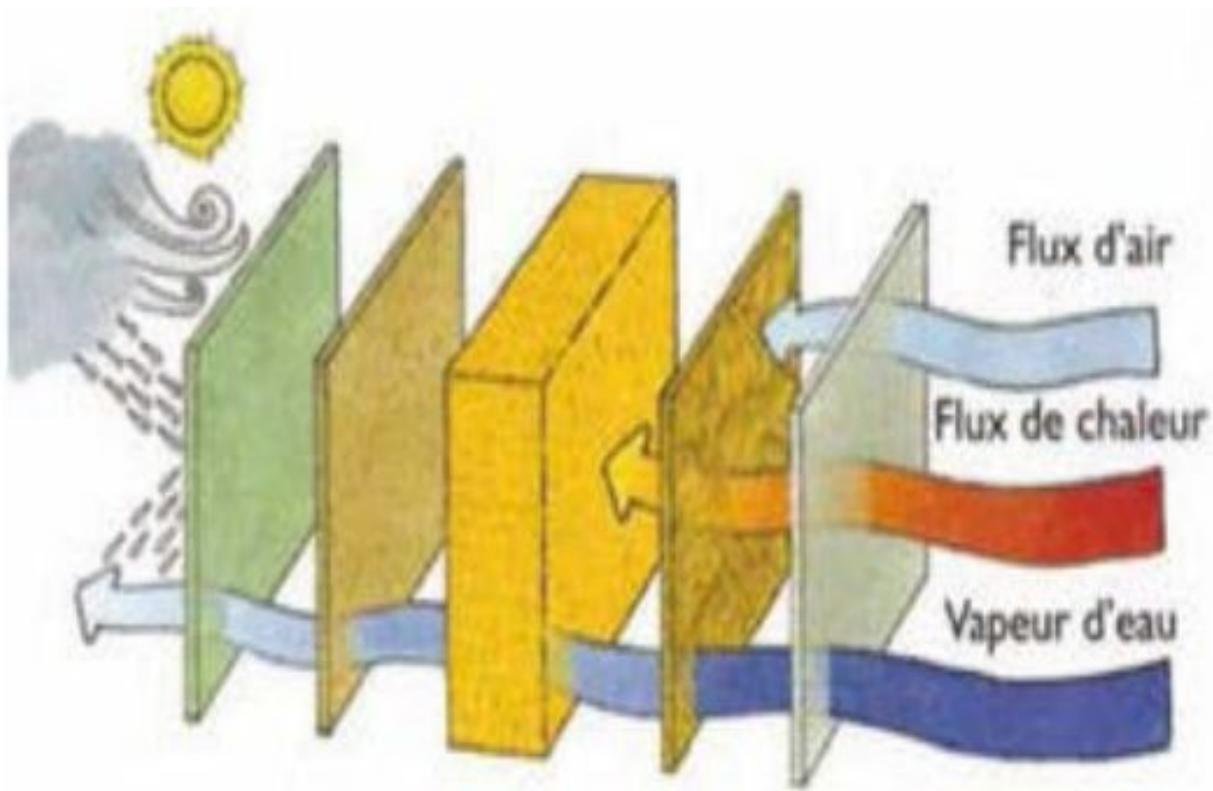
Up to 10% of annual global carbon emissions are stored in wood buildings.

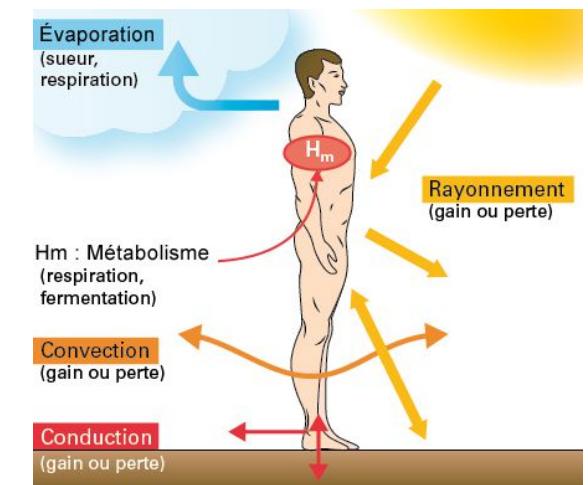
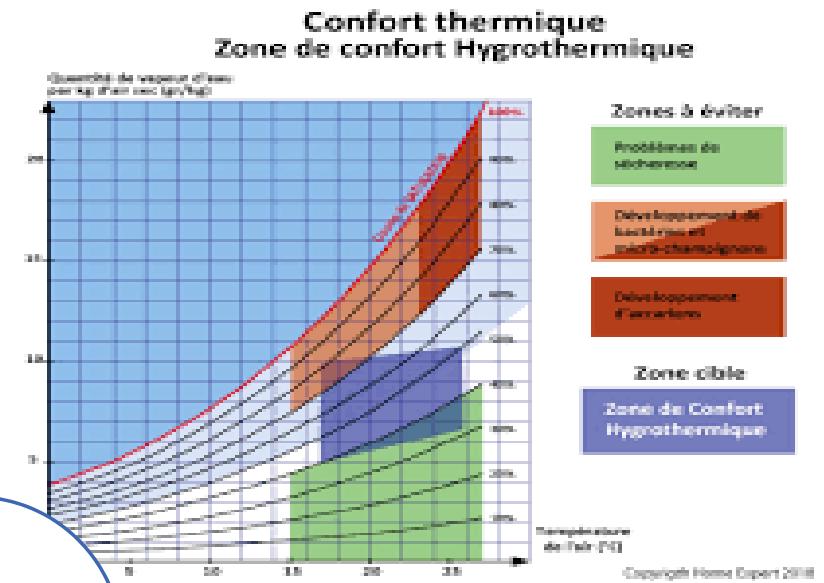
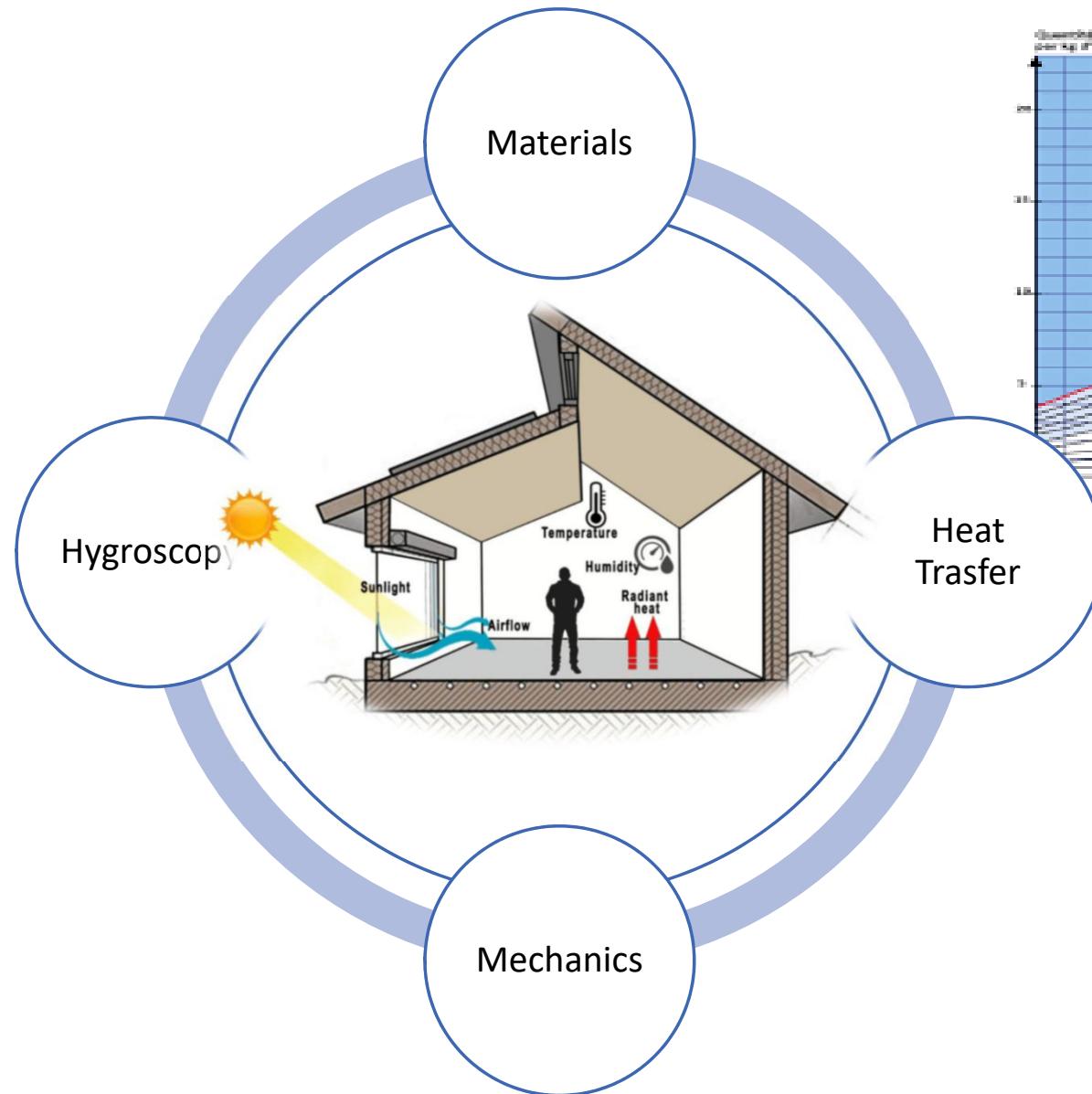
Architect
Andrew
Waugh
Immeuble
Londonien
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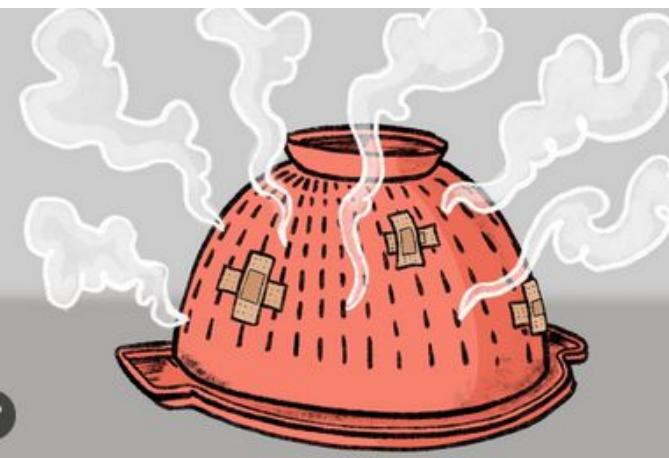




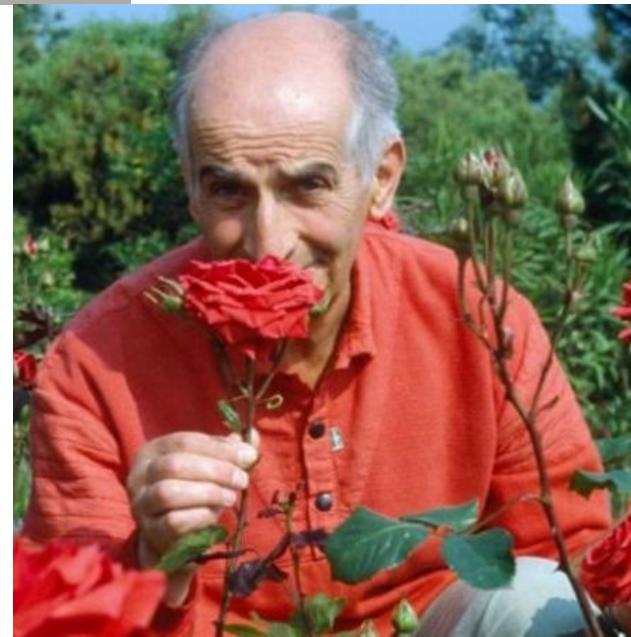
- The best form of carbon sequestration is to chop down trees: use the resulting wood as a building material and to restore sustainable, managed short rotation forests.
- The cost of durable wood finishing is very high and sometimes not environmentally friendly. New systems like UV Powder finishes could be interesting for high rise buildings where the cost is less determining.
- Could it be possible to replace all the coatings only by cell wall modifications?
- No Treatment could be a good treatment....with "Genetically Modified" wood!
- Genetically creating fast growing species with good durability is an ultimate dream!



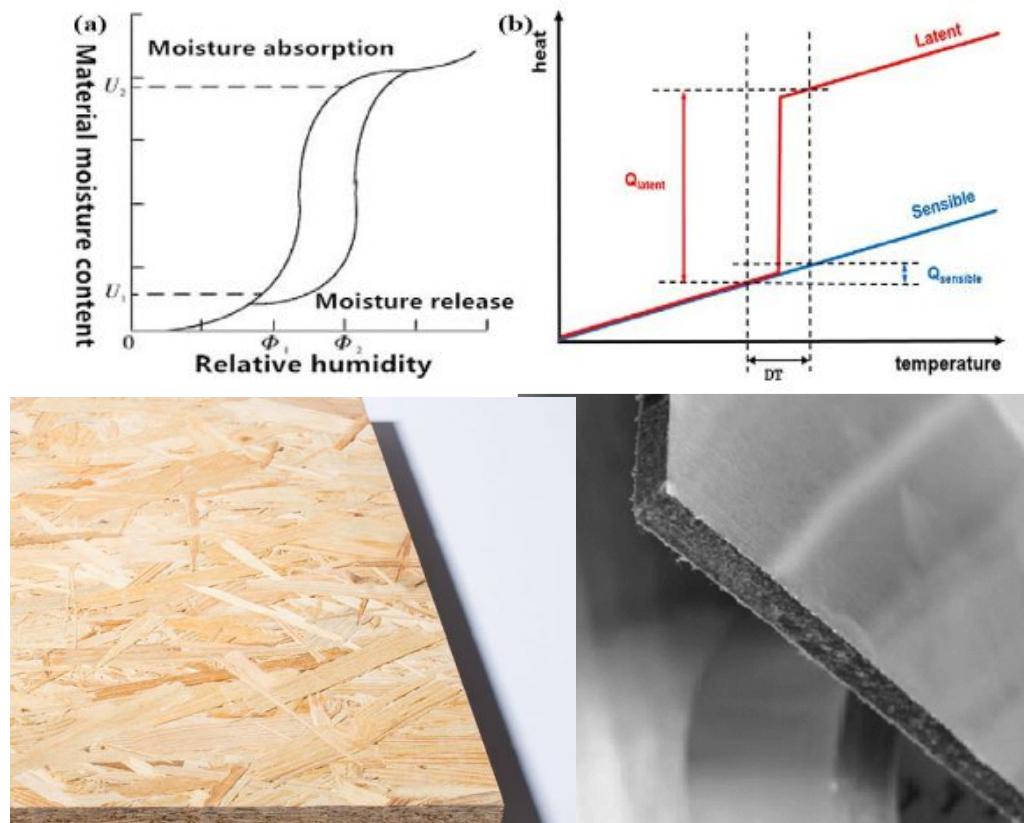




From RT 2012 to RT 2020



Hybrid / Combined solution



Photographie d'une plaque de MCP Energain (source : société Du- Pont de Nemours)

Maria Telkes

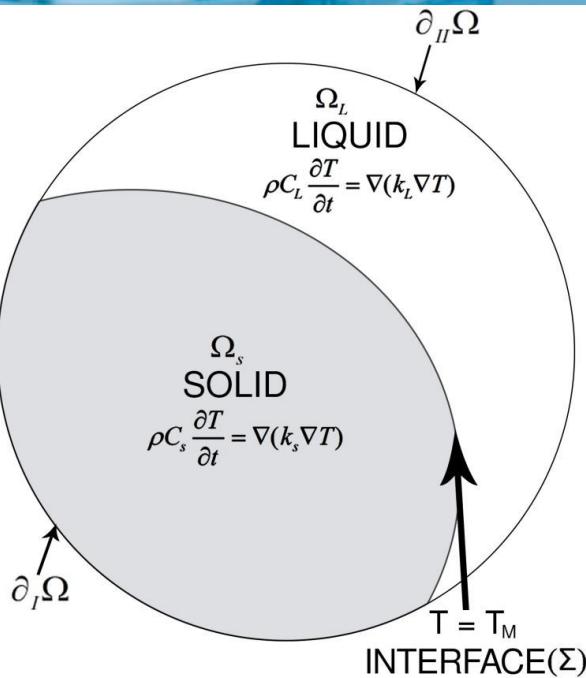


Mária Telkes 40's



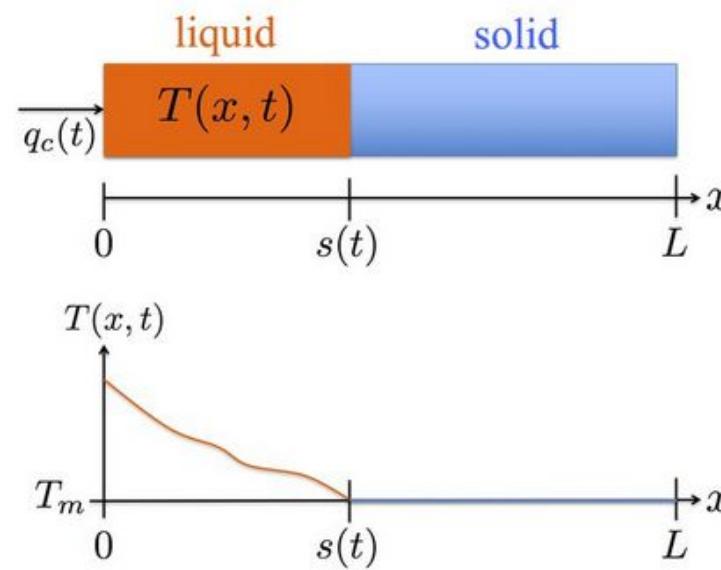
Construite à Dover dans le Massachusetts en 1948, cette « Maison de l'après-demain » est la première résidence moderne au monde à être entièrement chauffée grâce à l'énergie solaire.





- (1) One-dimensional planar symmetry, measured by the Cartesian coordinate x .
- (2) Constant specific heats $c_{\mathcal{P}}$, thermal conductivities $k_{\mathcal{P}}$, and diffusivities $\alpha_{\mathcal{P}}$, of the solid $\mathcal{P} = S$ and the liquid phase $\mathcal{P} = L$, together with the constant heat of fusion h_M .
- (3) Material properties of the phases could differ in general. The exception is the constant and equal density $\rho = \rho_S = \rho_L$ of the solid and liquid phases.
- (4) Heat flux $F_{\mathcal{P}}$ in phase \mathcal{P} is governed by the Fourier constitutive relation

$$F_{\mathcal{P}} = -k_{\mathcal{P}} \frac{\partial}{\partial x} T_{\mathcal{P}} \quad (1)$$



with $T_{\mathcal{P}}$ representing the temperature of the phase \mathcal{P} .

- (5) The temperature field $T_{\mathcal{P}}(x, t)$ at time t at point x is governed by the Fourier equation

$$\frac{\partial}{\partial t} T_{\mathcal{P}}(x, t) = \alpha_{\mathcal{P}} \frac{\partial^2}{\partial x^2} T_{\mathcal{P}}(x, t) \quad (2)$$

- (6) The solid–liquid interphase conditions at interphase point $x_M(t)$ at time t are

$$T_M = T_S(x_M, t) = T_L(x_M, t) \quad (3)$$

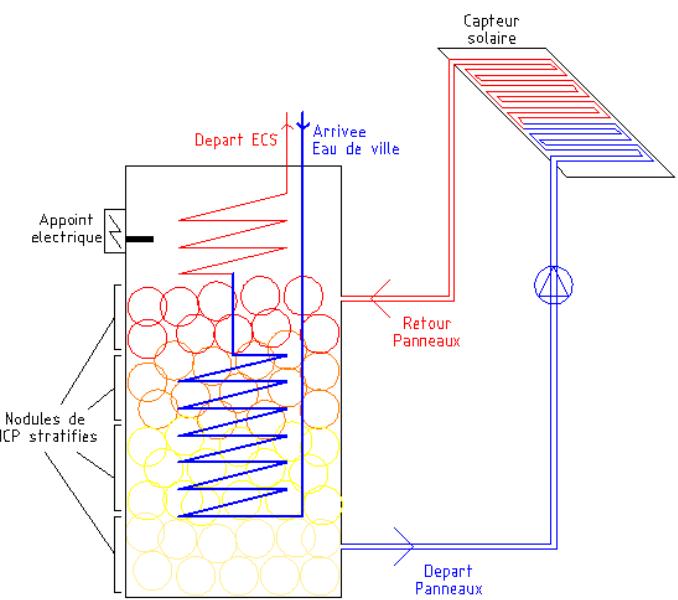
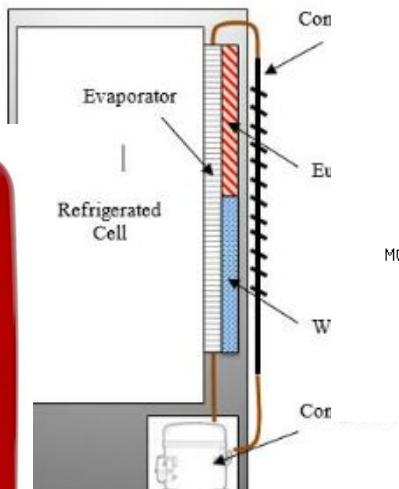
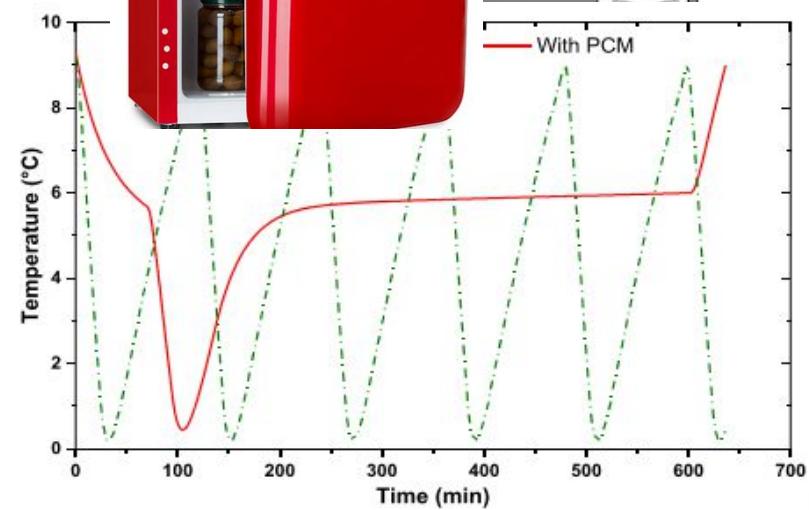
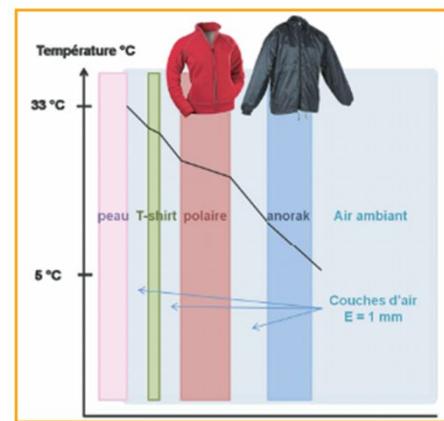
$$\rho h_M \frac{d}{dt} x_M(t) = -k_L \frac{\partial}{\partial x} T_L(x_M, t) + k_S \frac{\partial}{\partial x} T_S(x_M, t) \quad (4)$$

- (7) The temperatures of the phases are assumed to be in the general form

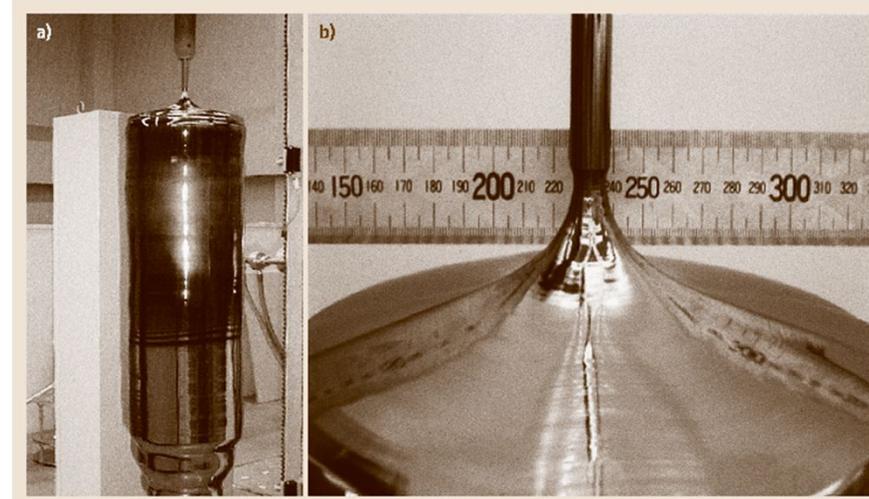
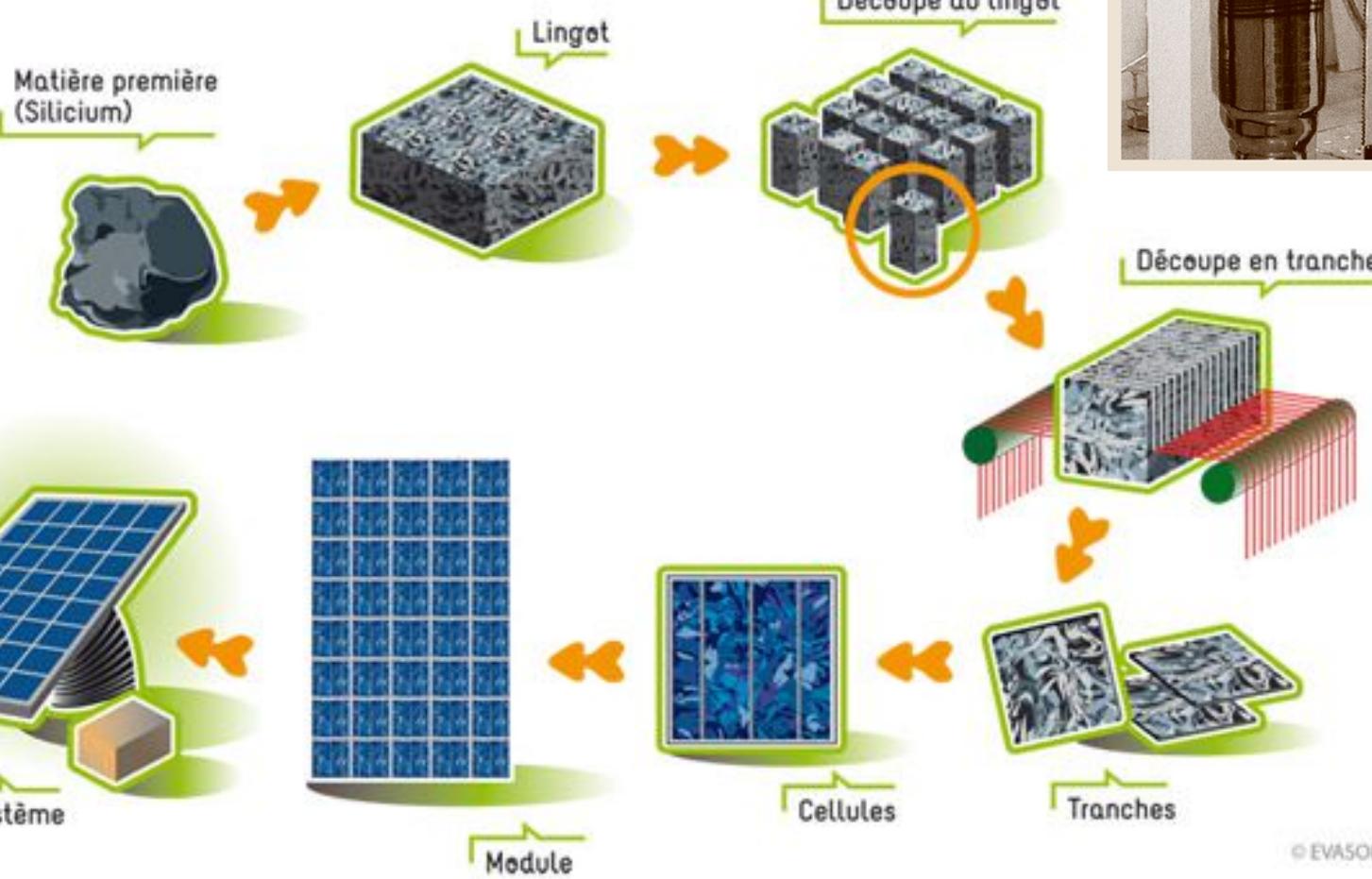
$$T_S = A_S + B_S \operatorname{erf} \left(\frac{x - x_0}{(4\alpha_S(t - t_0))^{1/2}} \right) \quad (5)$$

$$T_L = A_L + B_L \operatorname{erf} \left(\frac{x - x_0}{(4\alpha_L(t - t_0))^{1/2}} \right) \quad (6)$$

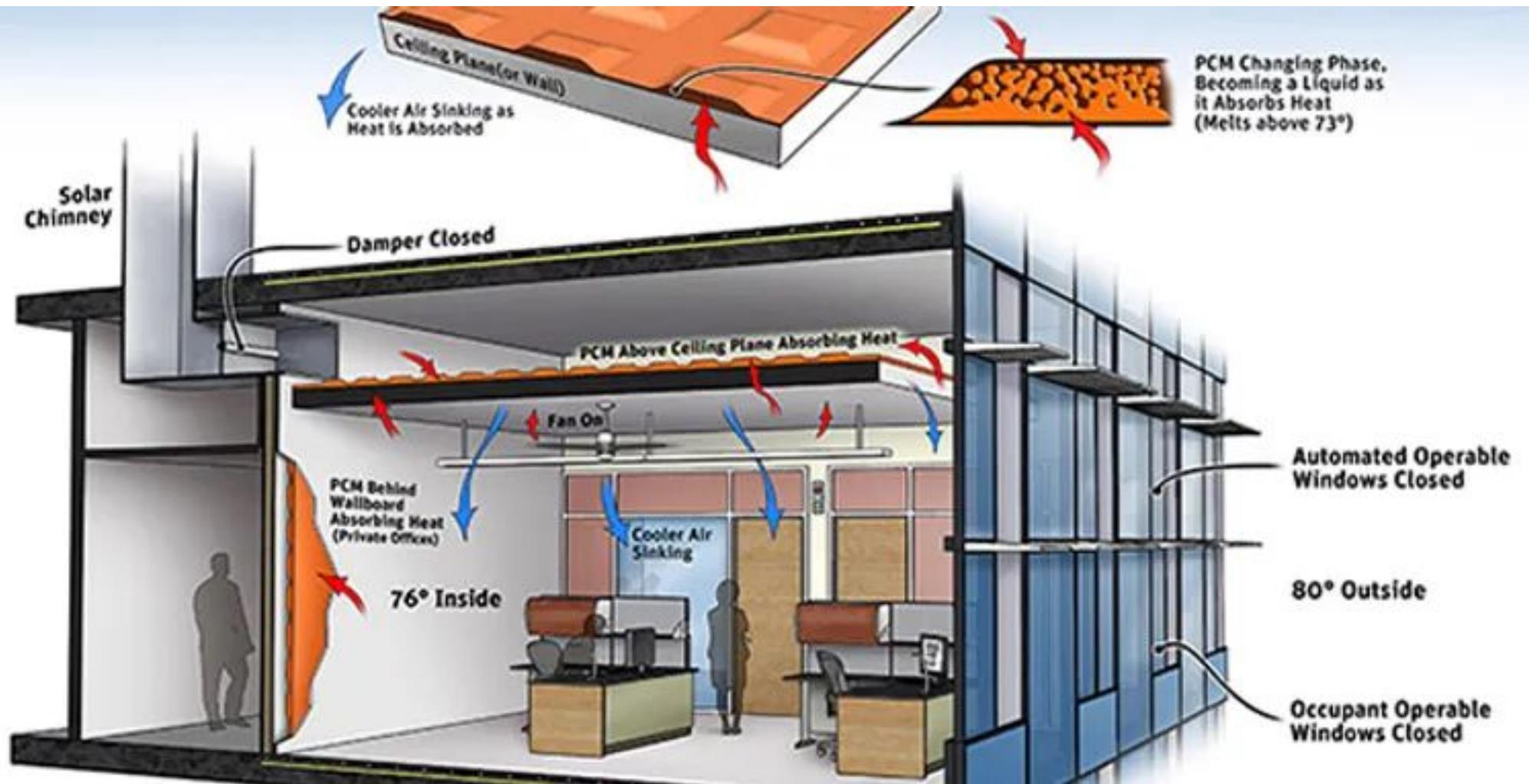
with the coefficients A_S , B_S , A_L , B_L , x_0 and t_0 , which have to be determined through the specific initial and boundary conditions.

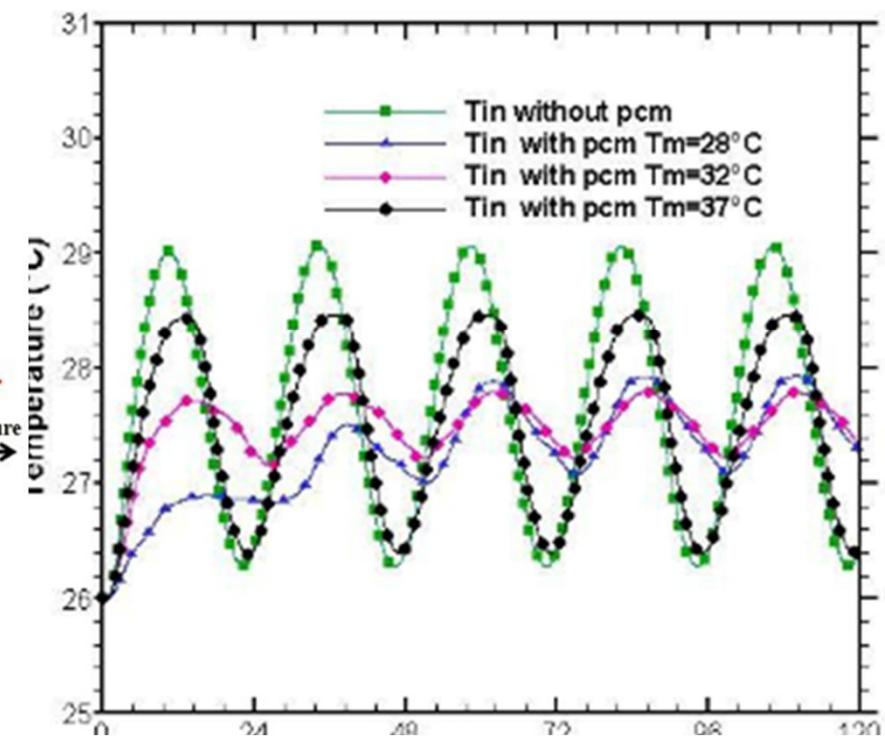
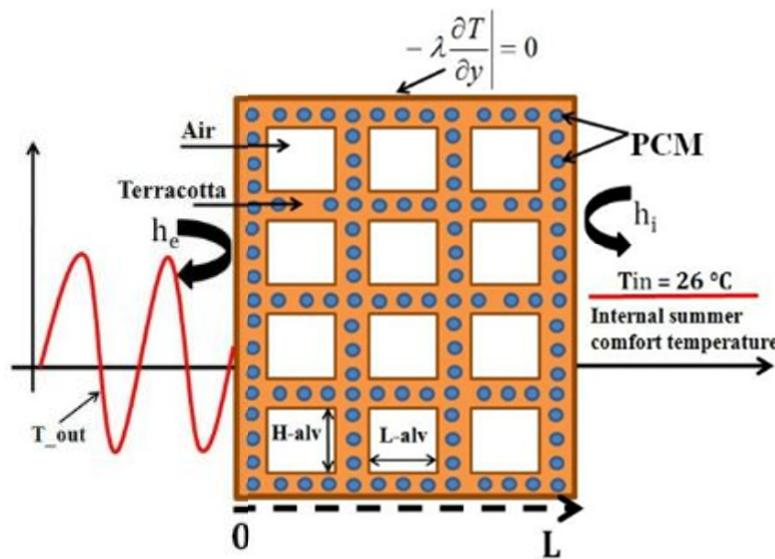
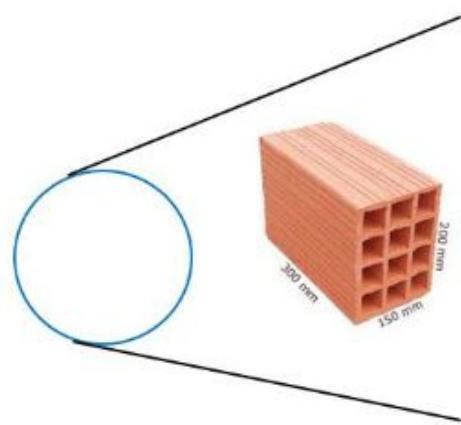
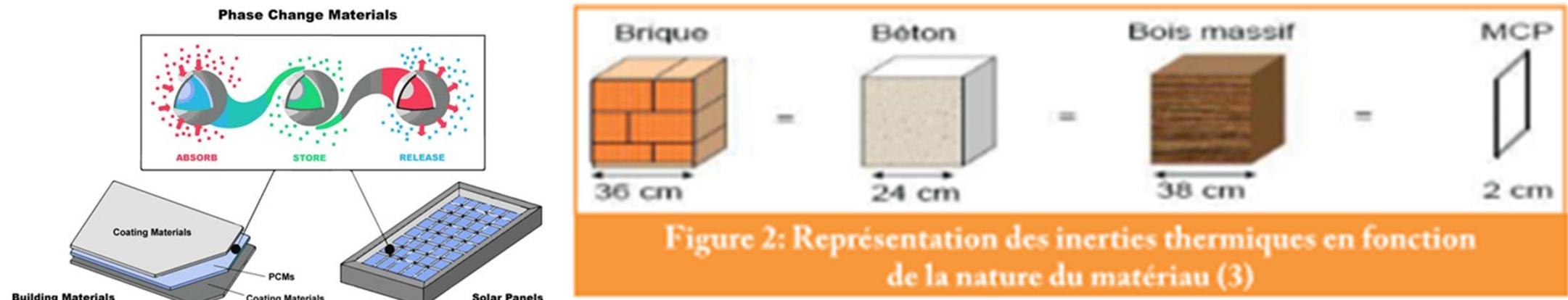


La chaîne de fabrication du photovoltaïque

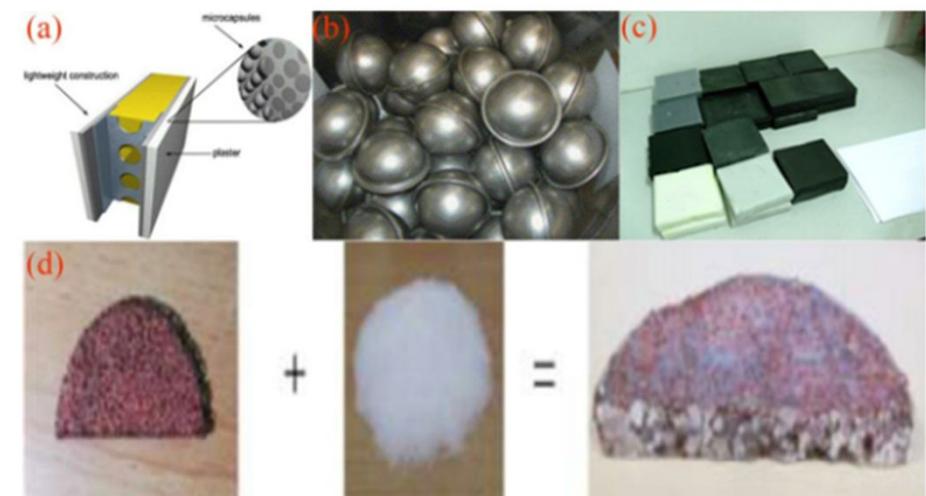
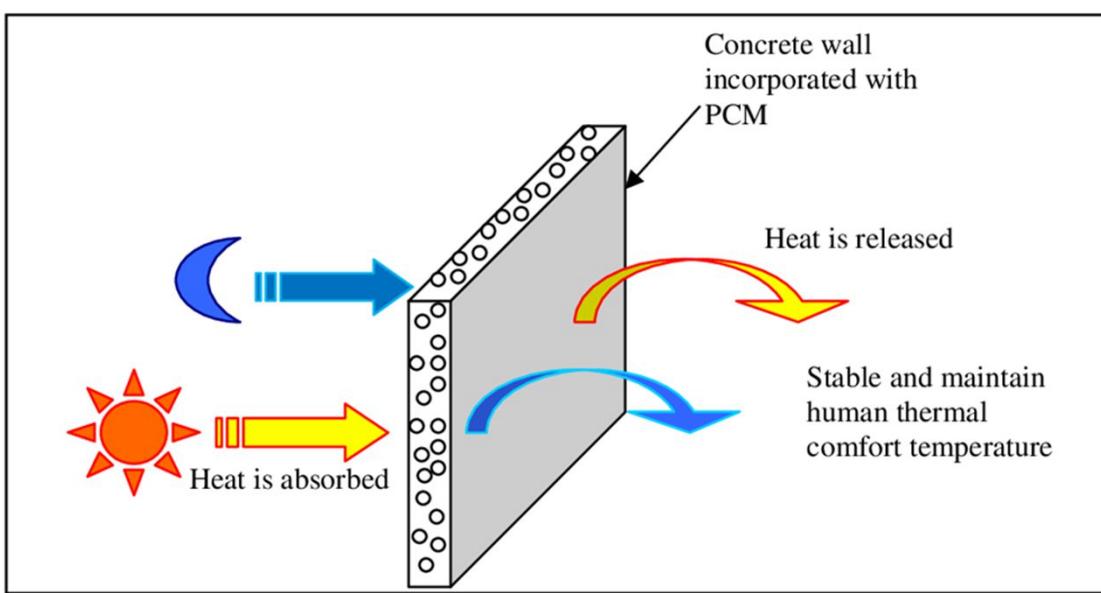
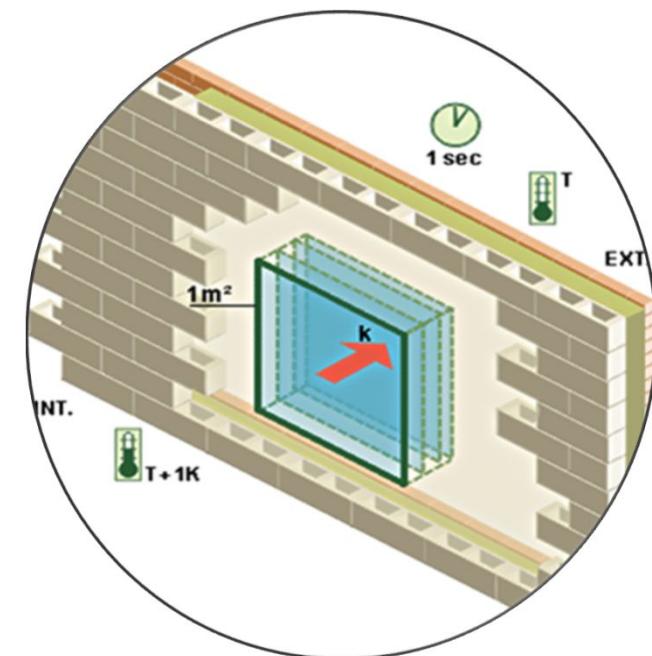
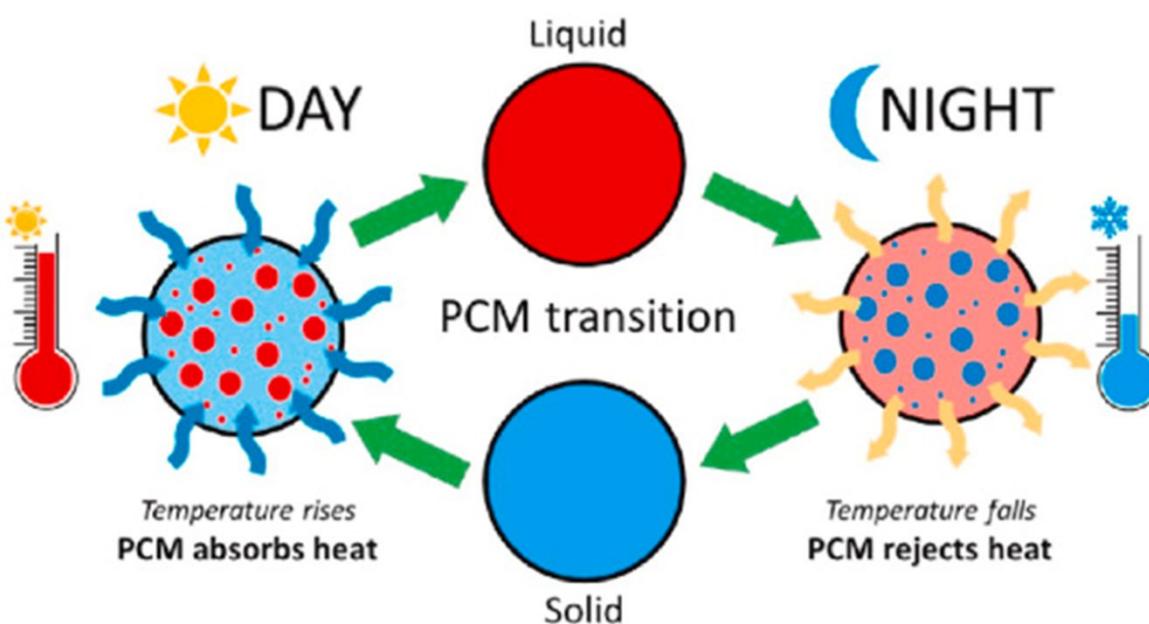


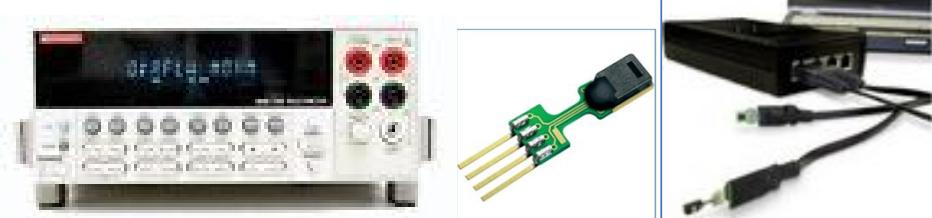
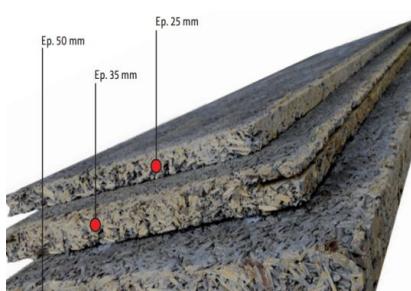
© EVASOL





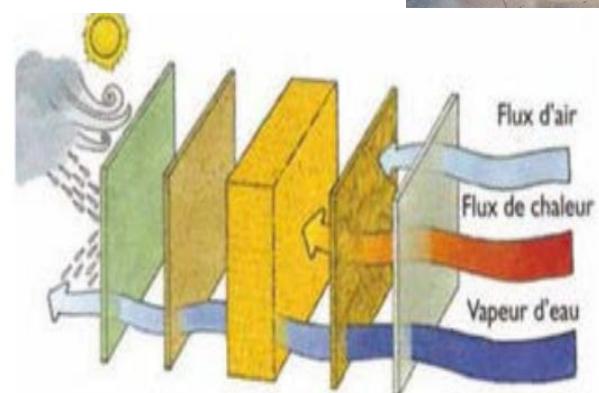
Mahdaoui, Pdoc



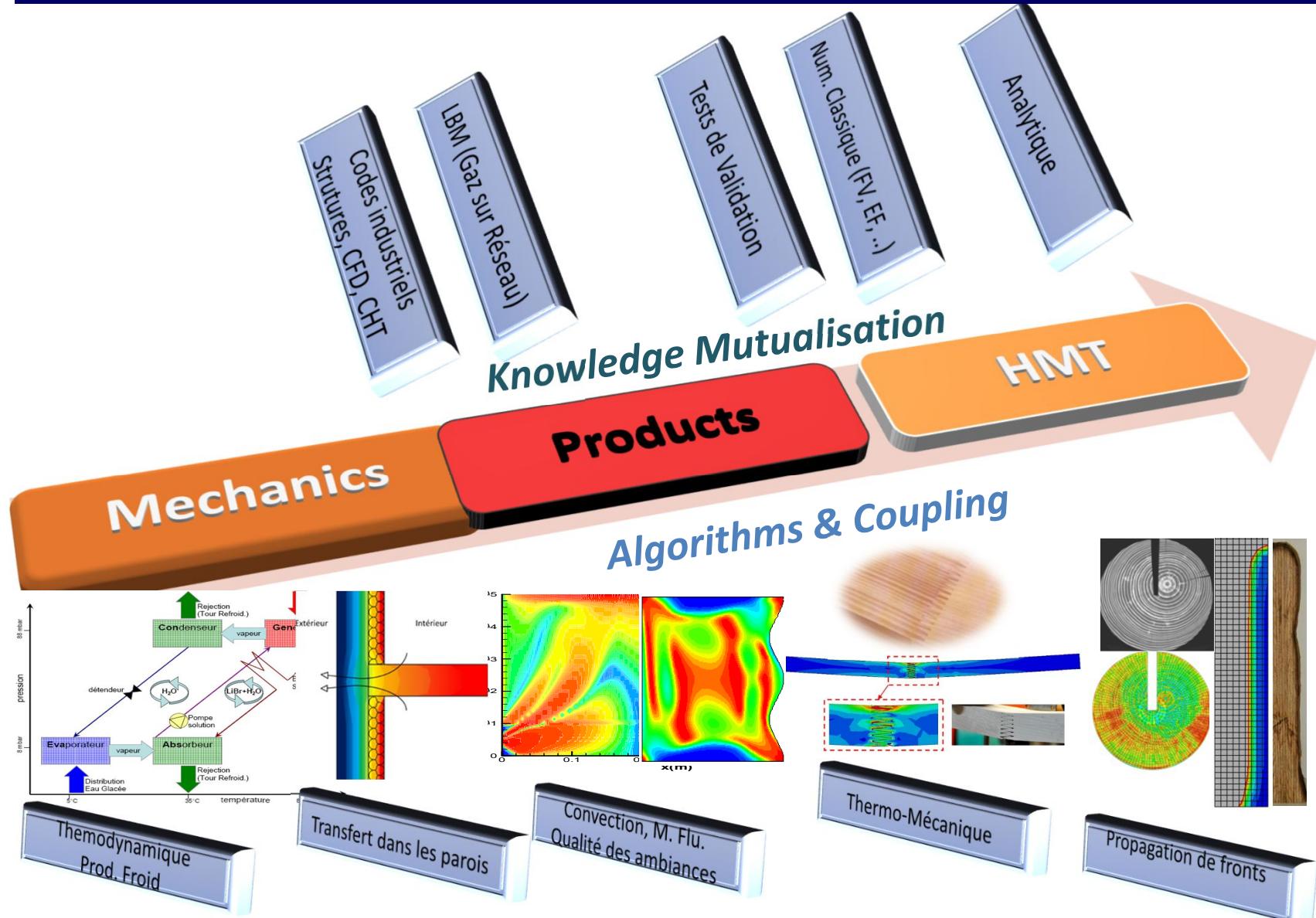




The inclusion experimental Loop



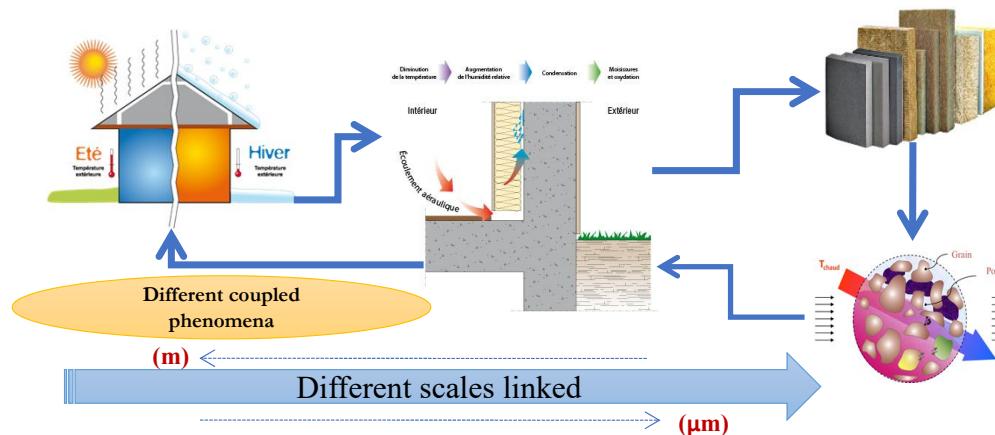
Understanding phenomena by modeling and simulation



Performance Of Biobased Materials In The Realization Of Sustainable Structures



- Analysis of coupled heat and mass transfers in building materials.
- Improving the energy performance of a building



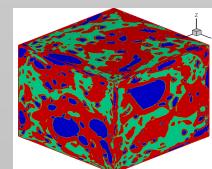
- ✓ The thermos-hydro behavior of the material was evaluated experimentally at material scale.
- ✓ The properties were used for numerical modeling at building scale.



Dr. MNASRI Faiza
Process and Product/
Energy Engineering

Microstructural Characterization

- ➔ Measuring equivalent properties:
- ✓ Characterization at the microscopic scale .
 - ✓ Modeling of thermohydric properties using numerical computation (3D reconstruction).



Orient the design of a new structure with controlled parameters.



LI Mengya
Doctorant en
Science de bois



UNIVERSITÉ
DE LORRAINE



Caractérisation expérimentale et modélisation des panneaux composites bois-ciment



Copeaux de bois
Ciment

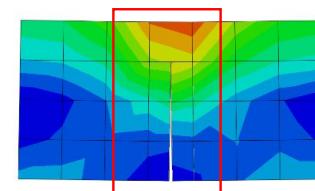


Composite bois-ciment

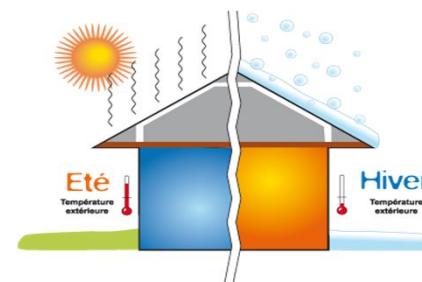


Coffrage permanent

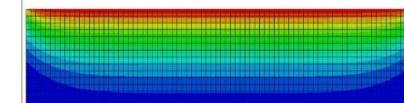
Comportement mécanique



Comportement hygrothermique



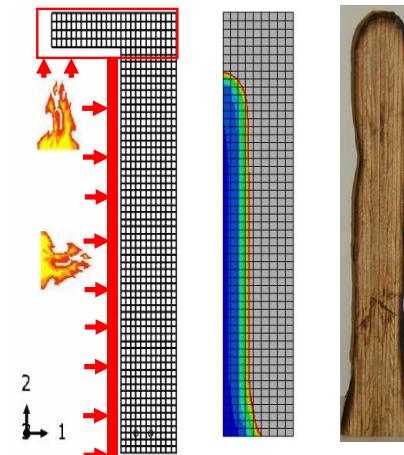
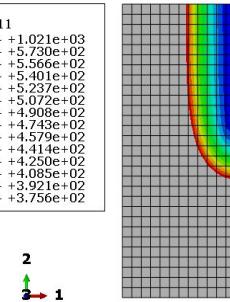
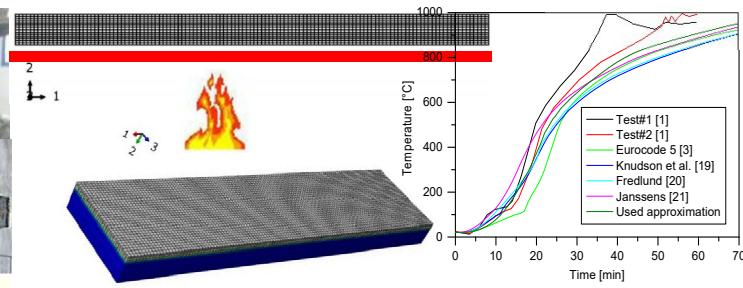
Comportement au feu



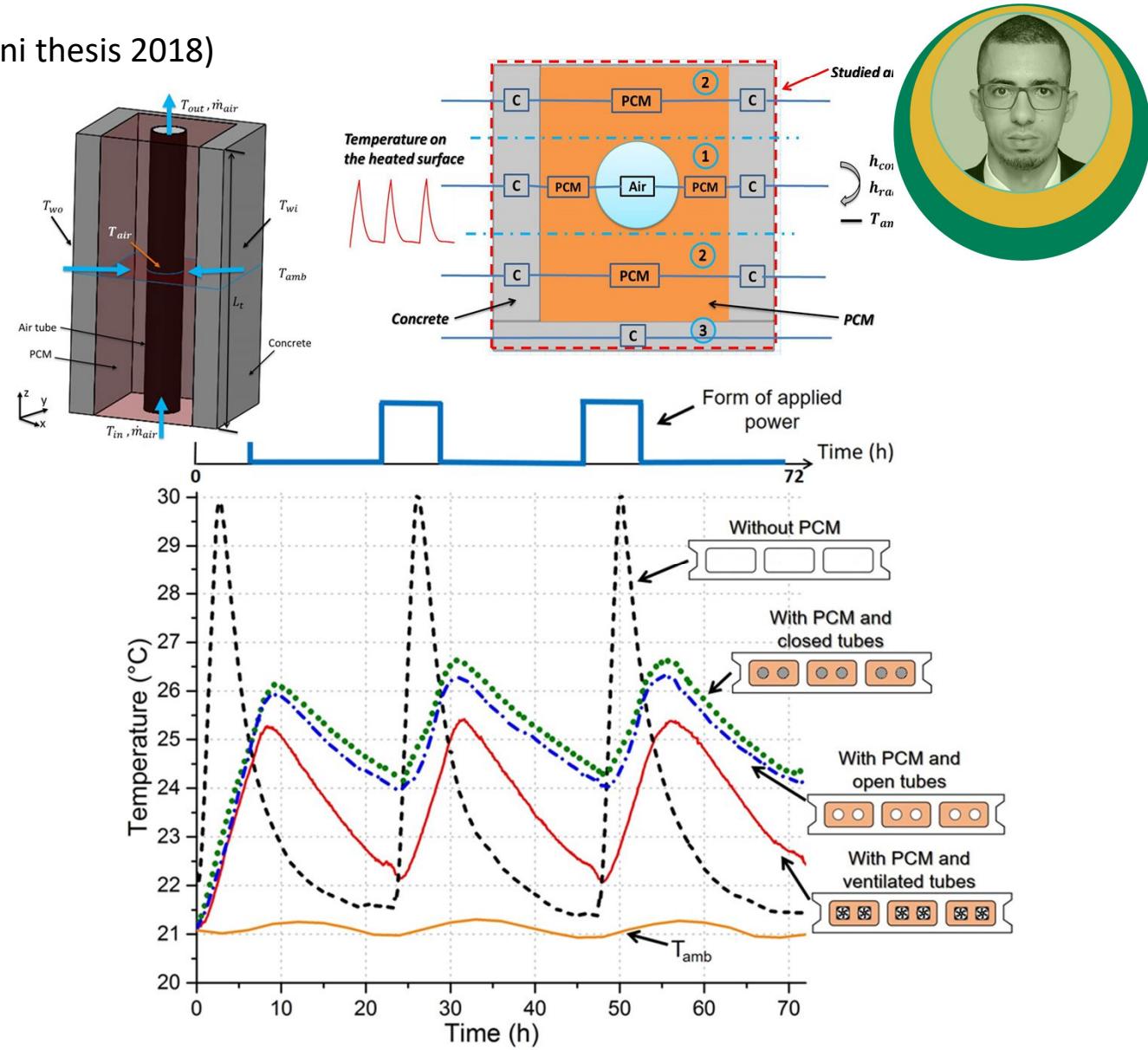
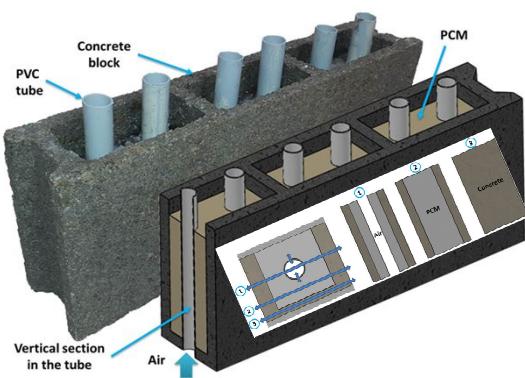


Dr. Thi Van Diem

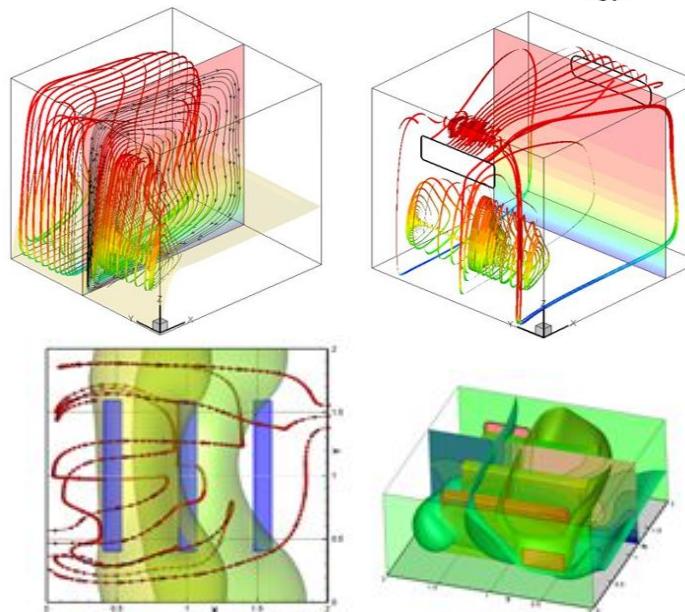
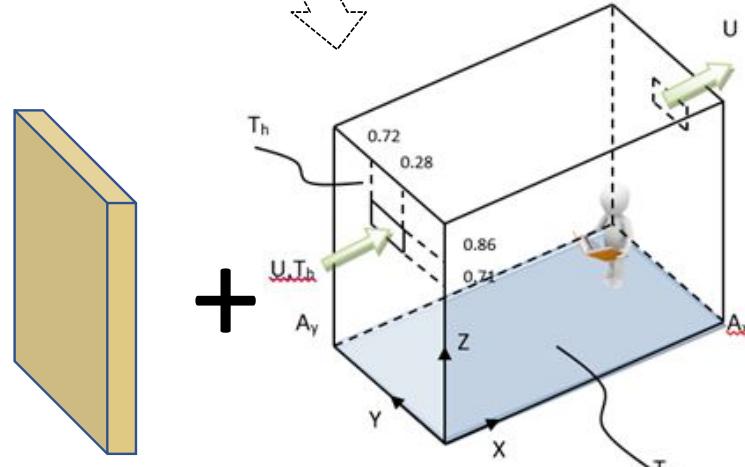
Pdoc

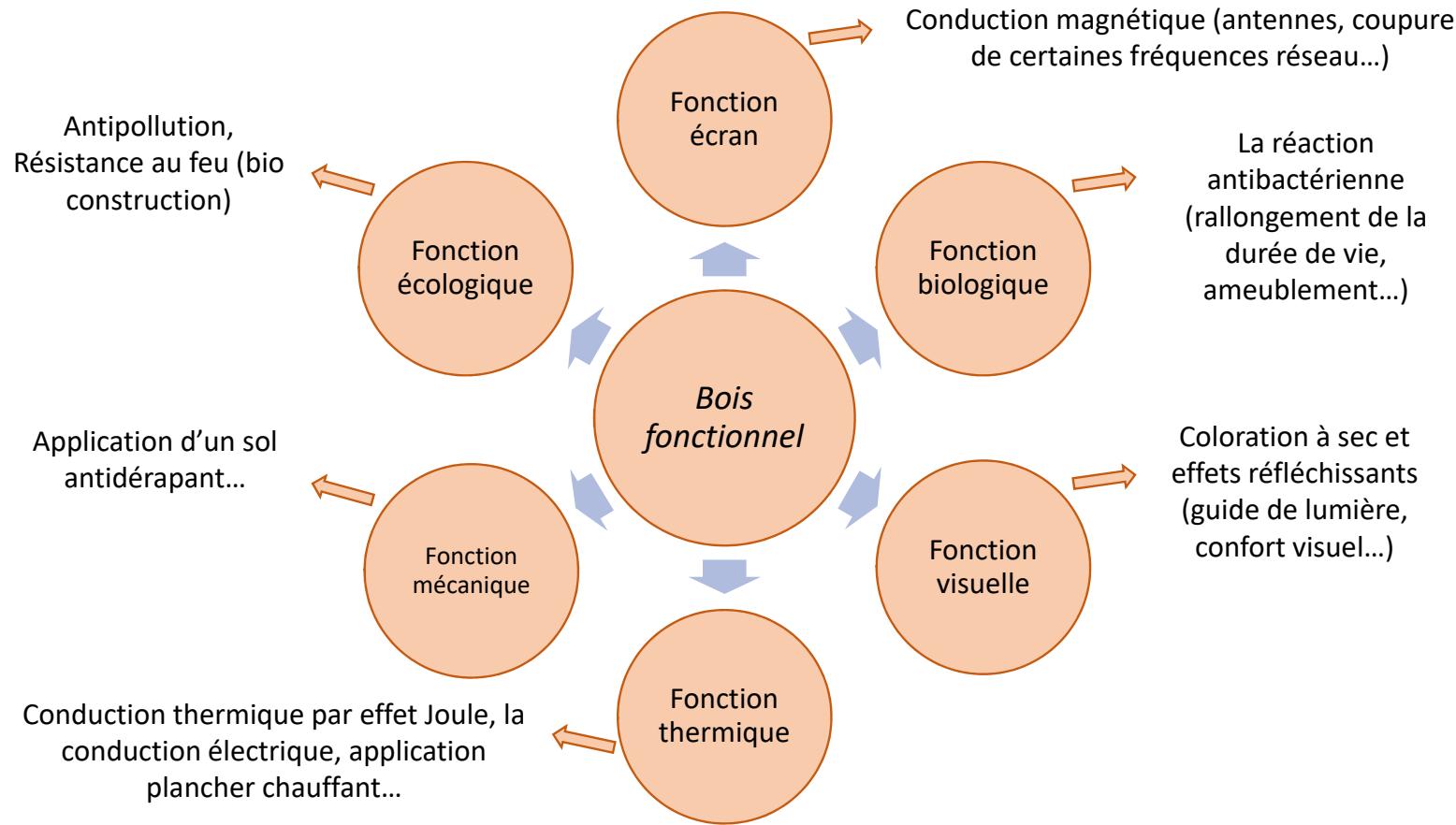


An Example of mixed solutions for Storage (Laouatni thesis 2018)



Project Tassili



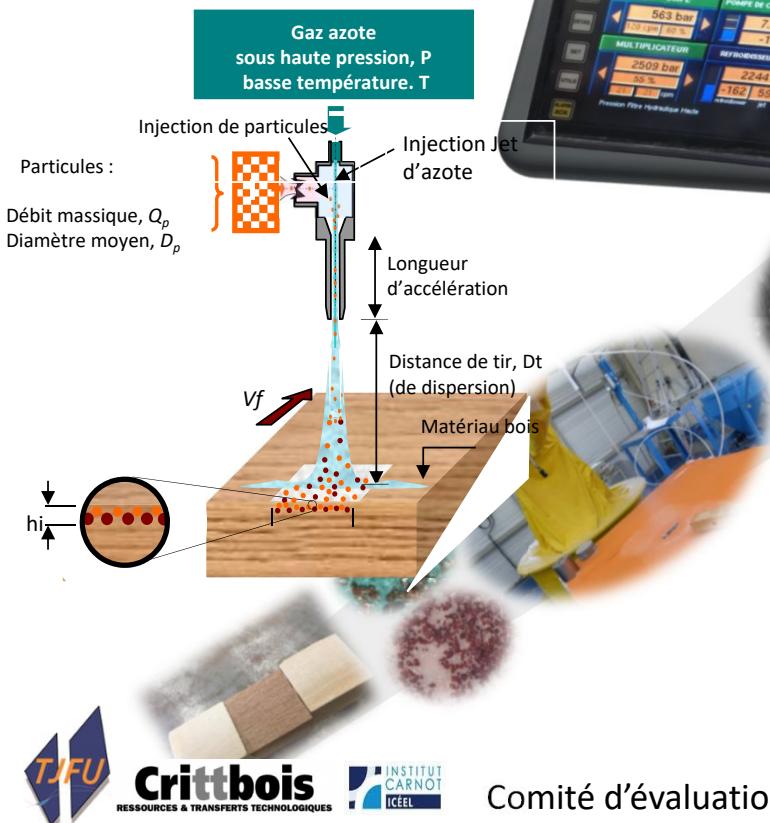


Fonctionnalisation de

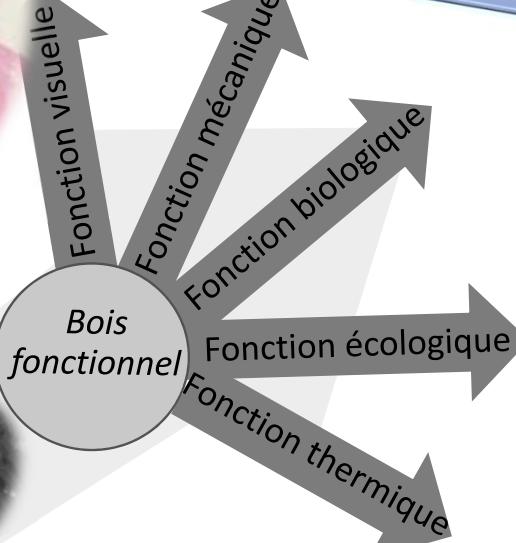
station de particules

Ch. Gérardin/M. El Ganaoui
Doctorat Mlle A. Zerria, en cours

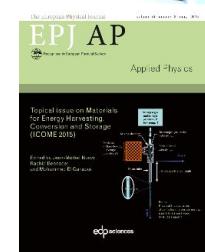
Méthode et procédé



Bois fonctionnel



Transversal Axes 1 - 3



Résultats

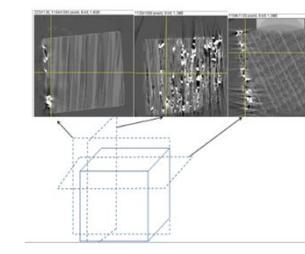
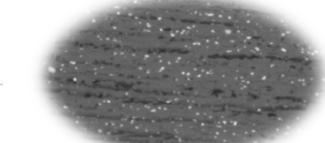


Image par
Tomographie



Sapin + Grenaille



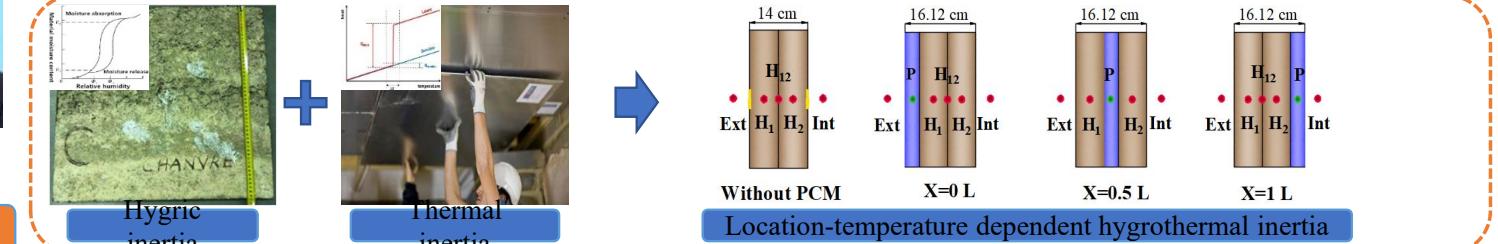
Peuplier + Cuivre



Dr. Dongxia
WU

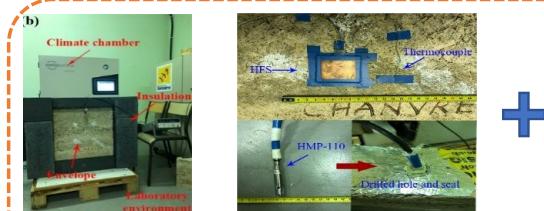
Motivation

Experimental and numerical study on passive building envelope integrated by PCM and bio-based concrete

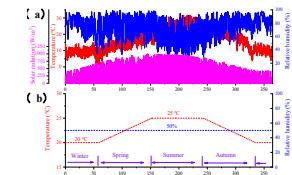


Location-temperature dependent hygrothermal inertia

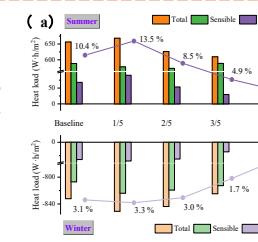
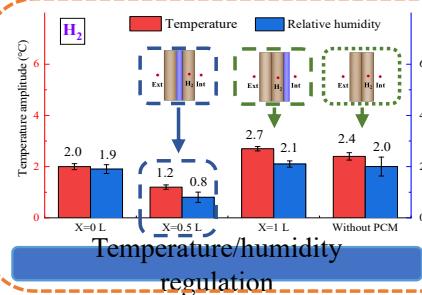
Methodology



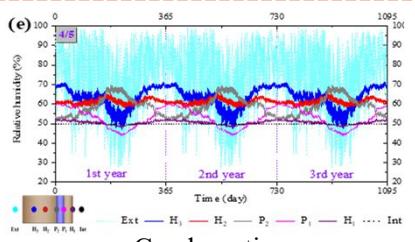
$$\begin{aligned} \xi_\varphi \frac{\partial \varphi}{\partial t} + \xi_T \frac{\partial T}{\partial t} &= \\ \nabla \left(\left(\delta_p p_{v,sat} + K_w \frac{\rho_w R T}{\varphi M_w} \right) \nabla \varphi + \left(\delta_p \varphi \frac{dp_{v,sat}}{dT} + K_w \frac{\rho_w R \ln(\varphi)}{M_w} \right) \nabla T \right) \\ \rho_{hc} C_{hc} \frac{\partial T}{\partial t} &= \nabla (\lambda_{hc} \nabla T) + L_v \nabla (D_{\varphi,v} \nabla \varphi + D_{T,v} \nabla T) \\ (\rho_{PCM} C^*) \frac{\partial T}{\partial t} &= \nabla (\lambda^* \nabla T) \end{aligned}$$



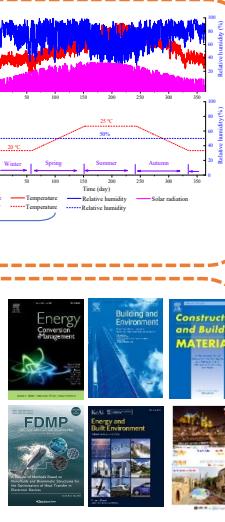
Simulation



Energy saving



Condensation avoiding



Publication



Dr. Thi Van Diem
Pdoc





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